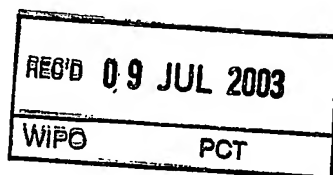




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- 3 JUL 2002

3. Full name, address and postcode of the or of each applicant (underline all surnames)

ROLLS-ROYCE plc
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GREAT BRITAIN

Patents ADP number (if you know it)

3970002

If the applicant is a corporate body, give the country/state of its incorporation

GREAT BRITAIN

4. Title of the invention METHOD AND APPARATUS FOR LASER WELDING

5. Name of your agent (if you have one)

"Address for service" in the United Kingdom
to which all correspondence should be sent
(including the postcode)

MR V J BIRD
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BS34 7QE

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a) any applicant named in part 3 is not an inventor, or

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Claim(s) 4

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Signature

Date

V J BIRD

3 JULY 2002

12. Name and daytime telephone number of person to contact in the United Kingdom PAUL WALKER 0117 979 7416
paul.walker@rolls-royce.com

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INSTRUMENT OF PATENT

- 1 -

DUPLICATE

METHOD AND APPARATUS FOR LASER WELDING

The present invention relates to laser welding. In particular, the present invention provides an improved apparatus and method for plasma suppression during laser welding.

According to a first aspect of the present invention there is provided a laser welding apparatus comprising, a laser, a laser head to focus a laser beam on a component to be welded, and plasma suppression means comprising gas supply means, wherein the plasma suppression means is arranged such that, in use gas is supplied to impinge the component at an angle between about 38° and about 52° to its surface, at a distance of at least 1mm from the intersection between the laser beam axis and component.

Preferably the laser welding apparatus comprises a laser head to focus the laser beam on the laser beam impingement point, and there is provided a nozzle adjacent the laser head that, in use, provides a jet of high velocity gas over the laser head.

Preferably, the apparatus further comprises a gas extraction means located adjacent the laser beam, diametrically opposite the plasma suppression means.

According to a further aspect of the present invention there is provided laser welding apparatus in which a laser beam is impinged upon a component to be welded at a laser beam impingement point wherein plasma suppression means is arranged to impinge a jet of gas on the component at an angle between about 38° and about 52° to its surface, flowing towards the laser beam impingement point, at a distance of at least 1mm from the laser beam axis.

Preferably, the plasma suppression gas is supplied to impinge the component at a point, which lies behind the laser impingement point in the welding direction.

Figure 2 shows a schematic cross section through the apparatus of figure 1 being used to carry out the method of the present invention.

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Turning now to figure 1, there is shown a component 2 mounted to a worktable 4. The worktable 4 has a cavity 6, beneath the component 2, in flow communication with an argon gas supply. Located above the table 4 is a laser head 8, which is mounted to a multi-axis computer numerically controlled (CNC) arm (not shown). The laser head 8 is in optical communication with a laser 10 via an optical conduit 12. For trials, a Haas HL3006 continuous 3kW Nd:YAG laser was used with a Trumpf TLC1005 work-handling device.

Turning now to figure 2, the laser head 8 and worktable 4 of the apparatus shown in figure 1 are shown during welding. The laser head 8 concentrates collimated laser light, generated by the laser 10, into a laser beam 14 with an axis 16 at a focus 18. A cover slide 20, transparent to the laser beam 14, protects the internal optics (not shown) of the laser head 8.

During welding, the laser head 8 is moved relative to the component 2 in a welding direction 22. At the focus 18 of the laser, the component 2 is melted and thermal conduction creates a molten pool 24 about this point. As the laser beam 14 moves in the welding direction 22, the molten material cools and solidifies, creating a weld 26, which trails the laser beam 14. During trials, the laser head 8 was kept a vertical distance of two hundred millimetres from the component 2, however this is not intended to be a limiting feature.

Plasma is generated as the laser beam 14 melts the component 2 and is ejected from the surface 28 of the component to form a cloud between the laser head and the component 2. In addition, particles are ejected from the molten pool 24. The plasma and particles both absorb energy from the laser beam 14, reducing the amount of energy reaching the component 2 and so reducing the depth of weld 26 that can be achieved. To reduce this effect, plasma suppression means 30 is provided in close proximity to the intersection 22 between the laser beam axis 16 and the upper surface 24 of the component 2 to remove the plasma from the vicinity of the component surface 28. The plasma suppression means 30 comprises a copper pipe 32 of eight millimetres internal diameter. The pipe 32 is in flow communication at a first end 34

with an argon supply (not shown), and open at a second end 36 to form a nozzle 36. The suppression means 30 is oriented at forty-five degrees to the surface 28 of the component 2. The nozzle 36 of the suppression means 30 points at the component 2 so that the centreline 38 of the pipe 32 intersects the surface 28 at a point behind the laser beam in the welding direction 22, four millimetres from the beam axis 16 in the horizontal plane. The exit of the nozzle 36 is raised from the surface 28 of the component 2 by a vertical distance of two millimetres.

During welding, argon gas is supplied to the plasma suppression means 30 at a flow rate of 14 litres per minute. The gas impinges the component surface 28 adjacent the weld pool and is deflected across the laser beam 14. The arrangement ensures that the gas does not significantly effect the molten pool 24, as this would reduce the quality of the weld. As the gas flow traverses the laser beam 14, it removes the plasma from the laser beam 14 path in the vicinity of the component 2.

Trials have shown that the plasma suppression means 30 works well over a range of parameters, although those described above are preferred. The copper pipe 32 may have an internal diameter of between about six millimetres and about ten millimetres and may be oriented to the component 2 at an angle of between about thirty-eight and about fifty-two degrees. The suppression means works well when the centreline of the pipe 32 intersects the component 2 at a point horizontally offset from the axis of the laser beam pipe between about one millimetre and about five millimetres, and with the nozzle vertically offset between about two millimetres and about five millimetres. Argon may be supplied at a rate of between about ten litres per minute and about eighteen litres per minute, or a different gas may be used such as carbon dioxide or another inert gas such as helium.

Gas extraction means 40 is located adjacent the laser beam 14 opposite the plasma suppression means 30. The extraction means 40 comprises a nozzle 42, adapted to suit the geometry of the component 2 being welded. For a flat component, the nozzle 42 comprises a rectangular opening ninety-five millimetres tall and seventy millimetres wide, scarfed at an angle of sixty degrees to the component surface 28. The nozzle is

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located fifty millimetres from the laser beam axis 16 in the horizontal plan, and two millimetres from the component surface 28 in the vertical plane at a point diametrically opposite the plasma suppression means 30. In operation, the nozzle extracts 80 cubic metres per hour of gas from the area surrounding laser beam 14, improving the velocity of argon gas across the laser beam 14.

A nozzle 44 with high width to depth ratio known as a 'spray head nozzle' is located adjacent the cover slide 20 in the horizontal plane, perpendicular to the laser axis 16. It comprises a horizontal row of sixteen, one millimetre internal diameter tubes 46. The tubes 46 are in flow communication at a first end 48 with a compressed air supply (not shown) and open at the opposite end 50 to form the nozzle 44. The exit of the nozzle 44 is offset five millimetres from the cover slide 20 in the vertical plane and offset ten millimetres horizontally. In operation, compressed air is supplied to the nozzle at sufficient rate to create a jet of compressed air travelling at thirty metres per second over the cover slide 20. The jet creates a traverse airflow beneath the laser lens to a depth of about one hundred millimetres, which protects the cover slide 20 from damage and which also removes any plasma not removed by the suppression means 30.

It is not intended that the invention should be limited to using a spray head nozzle 44 only as described above. The example given is a developmental model and it will be understood by the man skilled in the art that the salient features of the nozzle are that it has a flat aspect ratio, with a high gas flow velocity, causing a gas flow to some significant depth beneath the nozzle 44. This is quite unlike conventional 'air knives' used to protect the cover slide 18 of laser heads which are designed to minimise the disturbance to the atmosphere beneath them, between the laser head 8 and component 2. It will also be understood that compressed air is used as it is cheaper than using inert gasses, and contamination of the weld 26 is not likely given the distance therefrom. Nevertheless, it may be considered preferable to use an inert gas such as argon.

Together, the plasma suppression means 30 and spray head nozzle 44 work with the gas extraction means 40 to create a synergistic effect that removes plasma and other

particles from the laser beam 14 path to improve the depth of weld that the laser 10 can achieve. Trials using the apparatus hereinbefore described have shown a twofold increase in weld depth over conventional plasma suppression means for a given laser 10 power output. Nevertheless, it is envisaged that the system might be used without one of the features listed such as the gas extraction means 40.

To protect the weld from oxidation as it cools, oxidation suppression means 52 is located adjacent the plasma suppression means 30. The oxidation suppression means comprises a copper pipe 54 of thirteen and a half millimetres internal diameter. The pipe 54 is in flow communication at a first end 56 with an argon supply and open at a second end to form a nozzle 58 which is filled with Retemet 60, a porous metal compound. The oxidation suppression means 52 is oriented at forty-five degrees to the surface 28 of the component 2, with the nozzle 58 scarfed at a forty-five degree angle to the pipe axis so that the face lies parallel to the surface 28.

During welding argon is supplied, via the oxidation suppression means 54, to cover the weld 28 as it cools. The Retemet 58 ensures that the gas flow out of the nozzle 58 diffuses to cover the weld 28 evenly. At the same time, argon is supplied to the cavity 6 beneath the component to protect the underneath of the weld from oxidation.

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CLAIMS

- 1 Laser welding apparatus, in which a laser beam is impinged upon a component to be welded at a laser beam impingement point, wherein plasma suppression means is arranged to impinge a jet of gas on the component at an angle between about 38° and about 52° to its surface, flowing towards the laser beam impingement point, at a distance of at least 1mm from the laser beam axis.
- 2 Laser welding apparatus as claimed in Claim 1 wherein the laser welding apparatus comprises a laser head to focus the laser beam on the laser beam impingement point, and there is provided a nozzle adjacent the laser head that, in use, provides a jet of high velocity gas over the laser head.
- 3 Laser welding apparatus as claimed in Claim 1 or Claim 2 wherein the apparatus further comprises a gas extraction means located adjacent the laser beam, diametrically opposite the plasma suppression means.
- 4 Laser welding apparatus as claimed in Claim 1 wherein the plasma suppression means is adapted to supply gas to impinge the component at an angle of between about 38° and 52° .
- 5 Laser welding apparatus as claimed in Claim 4 wherein the plasma suppression means is adapted to supply gas to impinge the component at an angle of about 45° .
- 6 Laser welding apparatus as claimed in Claim 1 wherein the plasma suppression means is adapted to supply gas at a rate of between about 10 and 18 litres per minute.
- 7 Laser welding apparatus as claimed in Claim 6 wherein the plasma suppression means is adapted to supply gas at a rate of about 14 litres per minute.

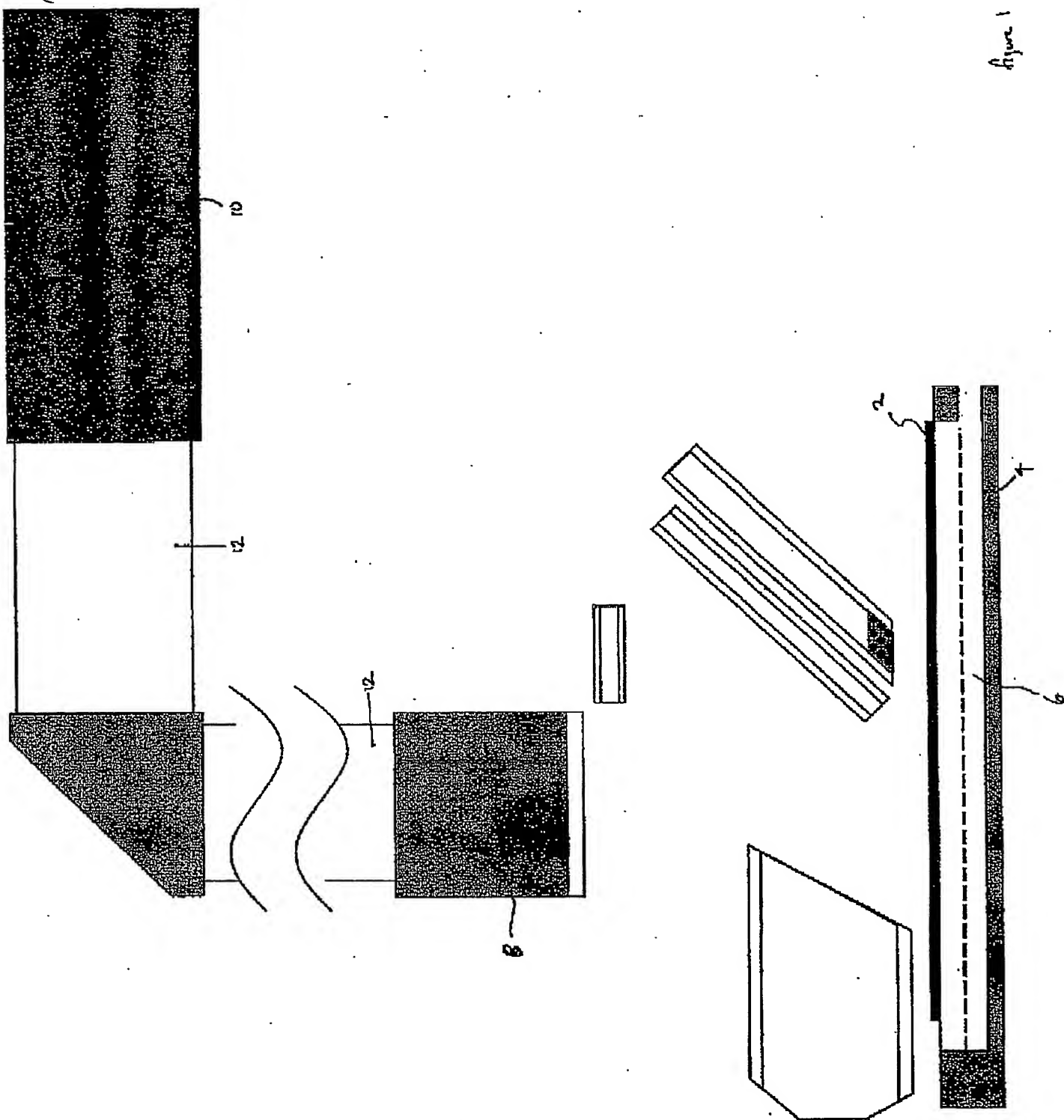
- 8 Laser welding apparatus as claimed in Claim 1 wherein the plasma suppression means comprises tubular supply means.
- 9 Laser welding apparatus as claimed in Claim 8 wherein the inner diameter of the tubular supply means is between about 6 mm and about 10 mm.
- 10 Laser welding apparatus as claimed in Claim 9 wherein the inner diameter of the tubular supply means is about 8 mm.
- 11 Laser welding apparatus as claimed in Claim 1 wherein the gas supplied by the plasma suppression means is an inert gas.
- 12 Laser welding apparatus as claimed in Claim 11 wherein the gas supplied by the plasma suppression means is argon.
- 13 Laser welding apparatus as claimed in Claim 1 wherein the plasma suppression means is adapted to supply gas to impinge the component at a distance of between about 1 mm and about 5 mm from the laser beam.
- 14 Laser welding apparatus as claimed in Claim 13 wherein the plasma suppression means is adapted to supply gas to impinge the component at a distance of about 4 mm from the laser beam.
- 15 Laser welding apparatus as claimed in Claim 1 wherein the plasma suppression means is arranged such that the gas exits the suppression means at a distance from the component surface of between about 2 mm and about 5 mm.
- 16 Laser welding apparatus as claimed in Claim 15 wherein the plasma suppression means is arranged such that the gas exits the suppression means at a distance from the component surface of about 2 mm.

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- 17 - Laser welding apparatus as claimed in claim 2 wherein the nozzle is a spray head nozzle.
- 18 Laser welding apparatus as claimed in Claim 2 wherein the high velocity gas exits the secondary supply means at, at least, 30 m/s.
- 19 Laser welding apparatus as claimed in Claim 2 wherein the exit nozzle of the secondary gas supply means is approximately 5 mm from the laser head.
- 20 Laser welding apparatus as claimed in Claim 2 wherein the exit nozzle comprises a row of small tubular outlets.
- 21 Laser welding apparatus as claimed in Claim 20 wherein the small tubular outlets all have an internal diameter of approximately 1 mm.
- 22 Laser welding apparatus as claimed in Claim 2 wherein the gas supplied via the secondary gas supply means is air.
- 23 A laser welding apparatus as claimed in Claim 3 wherein the gas extraction means lies between about 2 mm and about 5 mm from the surface of the component.
- 24 A laser welding apparatus as claimed in Claim 3 wherein the opening of the gas extraction means lies about 50 mm away from the axis of the laser beam.
- 25 A laser welding apparatus as claimed in Claim 3 wherein the gas extraction means is capable of extracting gas at a rate of about 80 m³/hour.
- 26 Laser welding apparatus substantially as hereinbefore described with reference to the accompanying drawings.

- 27 A method of laser welding a component the steps of, focusing a laser beam on substrate component, moving the component relative to the laser beam such that the laser beam impingement point moves in a welding direction, and supplying a plasma suppression gas to impinge the component adjacent the laser beam impingement point, wherein the gas flow is arranged to impinge the component at an angle of between 30° and about 60° to the component surface, and at a distance from the laser beam of at least 1 mm.
- 28 A method of laser welding a component as claimed in Claim AA wherein the plasma suppression gas is supplied to impinge at a point that lies behind the laser impingement point in the welding direction.

Figure 1



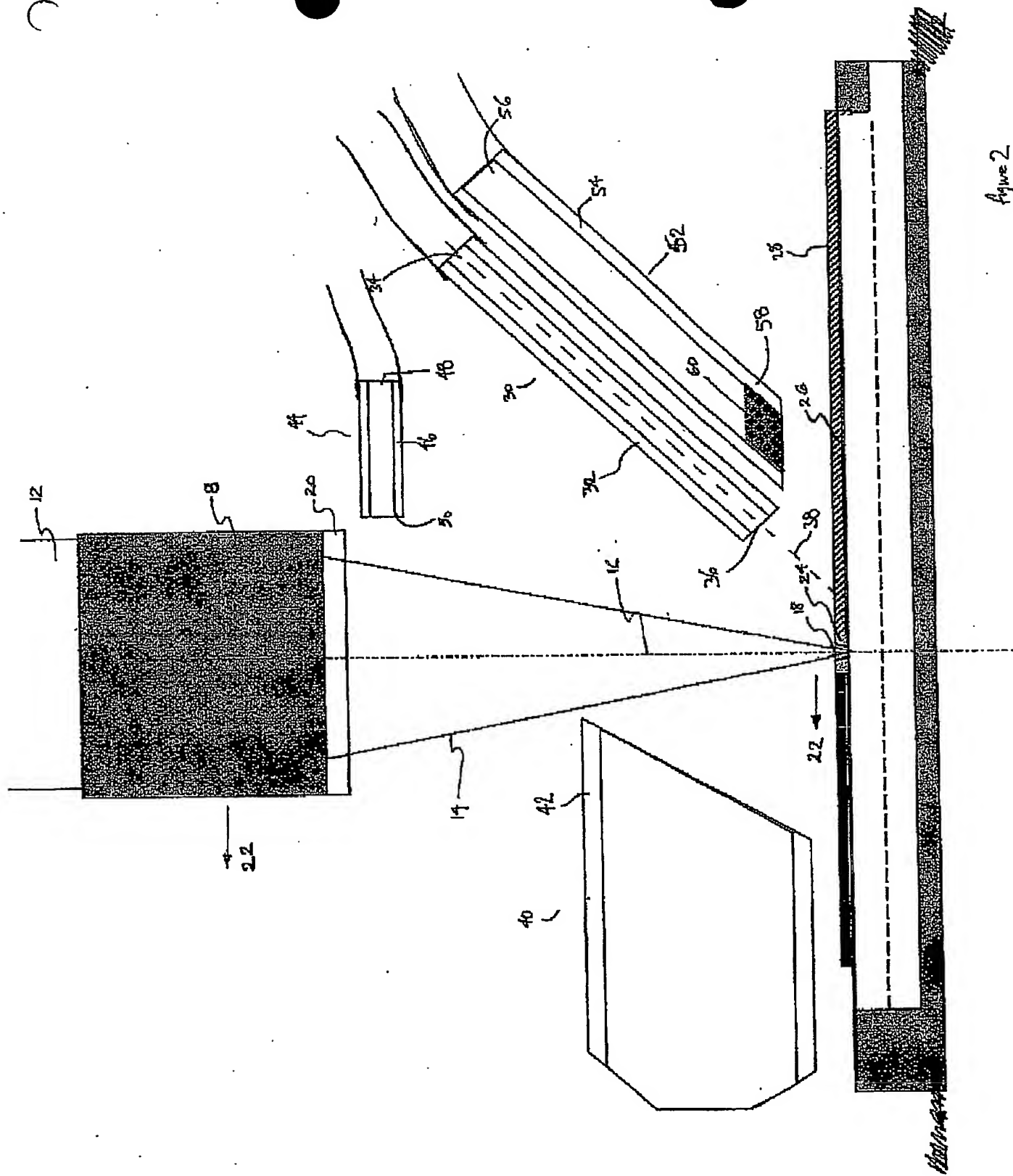


Figure 2

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